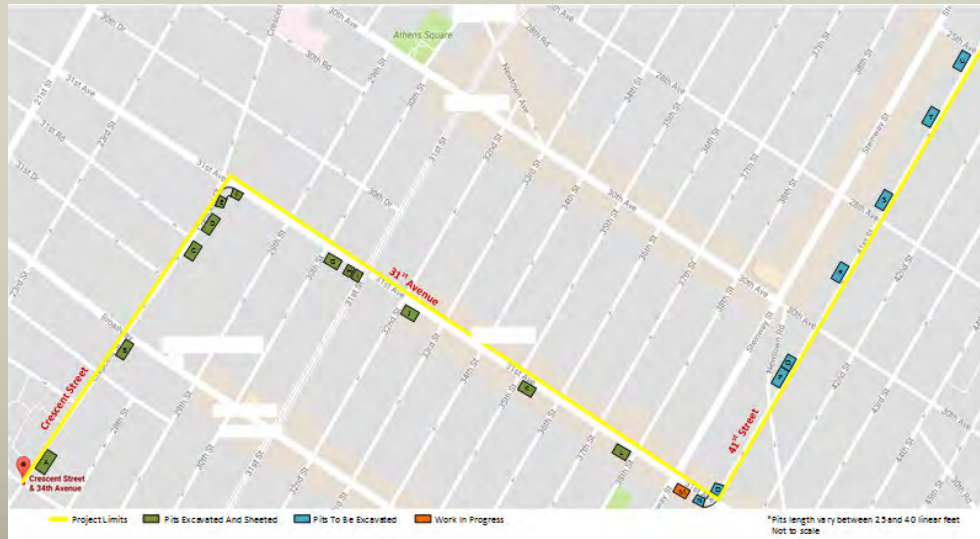




NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY

STRATEGIC SLIP LINE REHABILITATION OF NEW YORK CITY'S TRUNK WATER MAIN SYSTEM



MARIO VALENTI, P.E.

THOMAS M. LEUNG, P.E., ESQ.



**Department of
Design and
Construction**

Executive Summary

Objective: To reactivate a major trunk water main system after over 20 years of discontinued service and connect to the newly activated Water Tunnel No. 3.

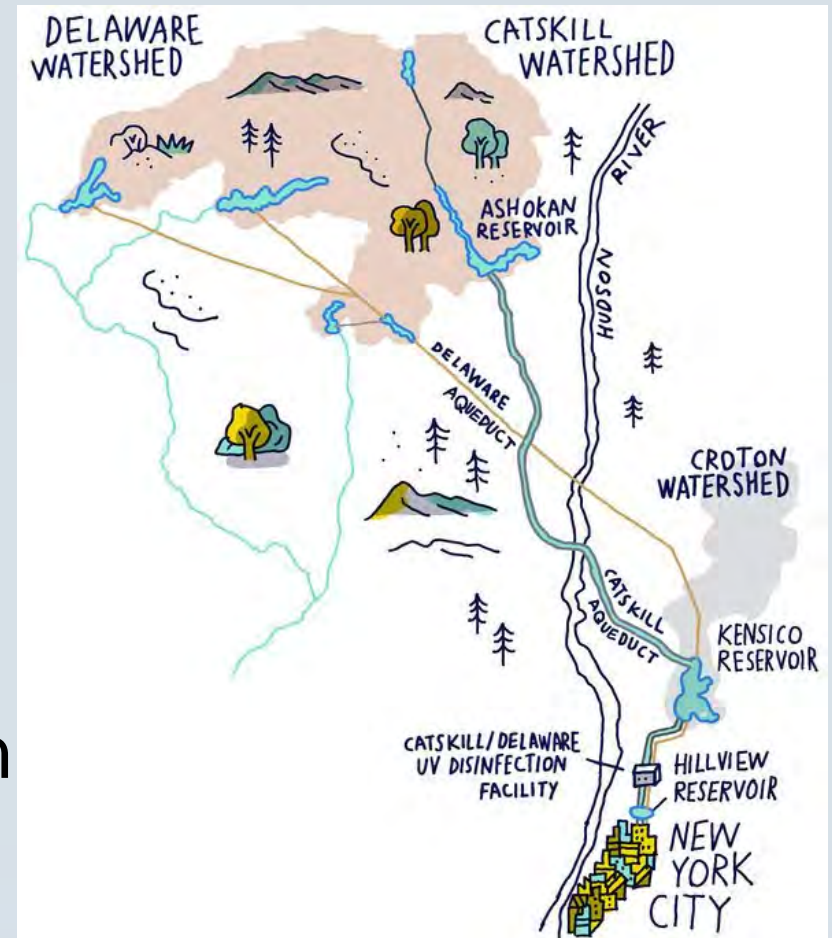
Means & Method: Slip Line through 17 densely populated city blocks (7,016 LF) in Astoria, Queens.

- Liner Pipe is 52" O.D.
 - 1/2" wall steel pipe with mortar interior and polyurethane exterior coatings.
- Host Pipe is 60" I.D.
 - 5/8" wall steel pipe with coal tar interior and exterior coating.
- Slip Line Installation includes:
 - 16 individual runs ranging in length from 81.5' to 773'.
- Open-Cut Restoration **limited** to
 - approximately 1,100 lf of 52"/60"/72" steel pipe and appurtenances.
- Reduce construction duration and cost by at least **50%** as compared to Open-Cut.



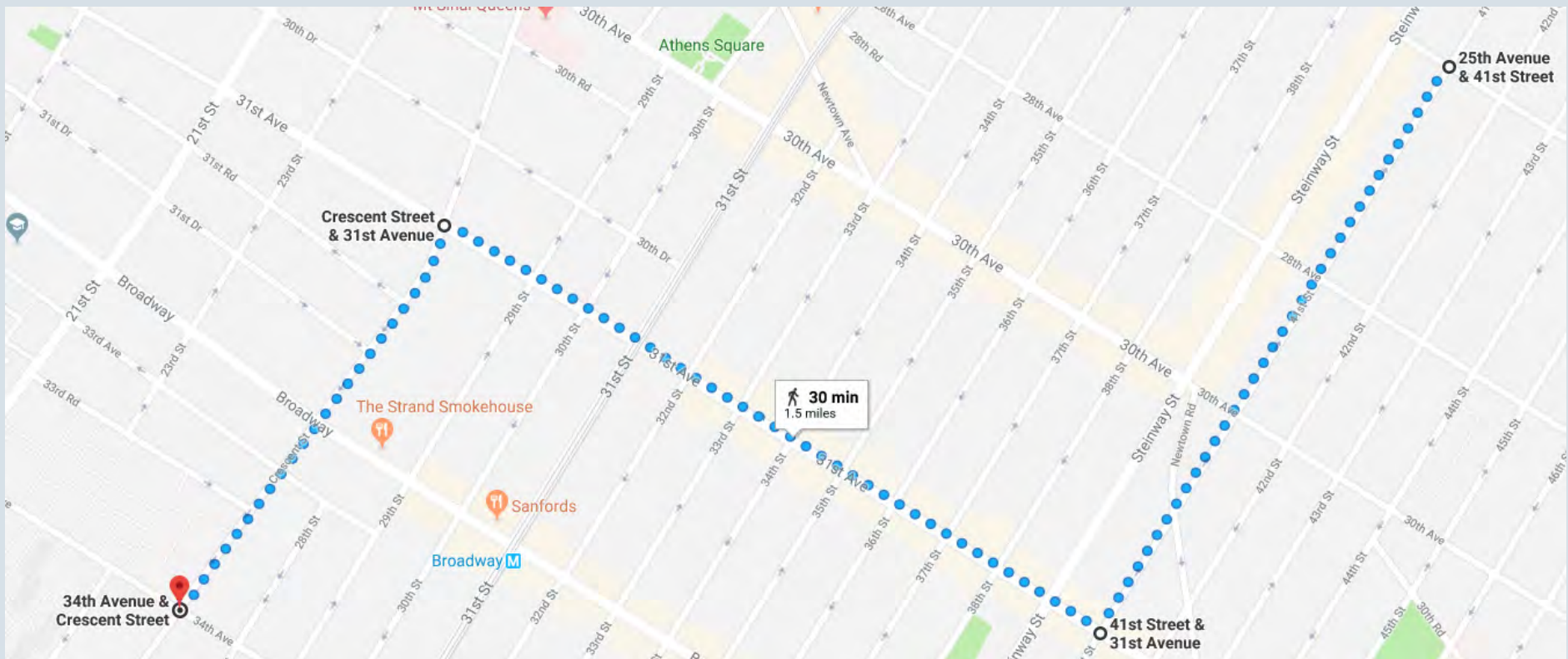
Background of NYC's Water Distribution System

- Two Reservoirs
 - Catskills and Croton
- Three Water Tunnels
 - Nos. 1, 2 and now 3
- Water Tunnels → Shafts
- Shafts → Trunk Mains
- Trunk Mains → Distribution



History of 60" Trunk Water Main

- Installed in Astoria, Queens, in 1989.
- Failed in January 1996.
- Low temperature + Low ductility → **Failure!**



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Chemical Analysis Results

- Low, but within tolerances:
low Manganese
low Molybdenum
+ low Chromium

While acceptable individually,
the low combination of the three
resulted in disaster

60" STEEL WATER MAIN IN ASTORIA Failed Jan. 02, 1996					
SUBJECT: ANALYSIS OF CARBON STEEL FROM FAILED WATER MAIN ASTM A283-88, GRADE C					
Laboratory Nos.: 37919-20					
Represents: Spiral-welded pipe from a broken 60" water main at the intersection of 31 st Avenue & 33 rd Street, Astoria, Queens. The break occurred on January 2, 1996. The pipe was fabricated by Progressive Fabricators, St. Louis, MO under Contract 522B and was to conform to the specifications of ASTM 283, Grade "C" as modified by the Contract. The samples were received from George Andersen, Administrative Engineer II, BWS & WC. Sample No. 37919 is from the bell section whereas Sample No. 37920 is from the spigot end of the adjoining pipe. The samples were analyzed for carbon and sulfur by combustion; all other elements were analyzed by using X-ray fluorescence.					
	(BELL) #37919	(SPIGOT) #37920	Percentage Composition ASTM A283-88, Gr. C Specifications	Contract 522B Modifications	
→ Carbon	0.20	0.19	0.24 max.	no requirement	
→ Manganese	0.40	0.71	0.90 max.	no requirement	
→ Phosphorus	0.008	0.003	0.04 max.	0.04 max.	
→ Sulfur	0.027	0.026	0.05 max.	0.05 max.	
→ Silicon	0.01	< 0.01	0.40 max.	no requirement	
→ Copper	0.02	0.03	----	0.15 max.	
→ Nickel	0.02	0.03	----	0.15 max.	
→ Molybdenum	< 0.01	< 0.01	----	0.07 max.	
→ Chromium	0.04	0.02	----	0.09 max.	
Consequently, the material analyzed meets the chemical specification limits of both ASTM A283-88 and Contract 522-B.					



Charpy V-Notch Results

60-Inch Water Main, Astoria, NY 1996											
WMAR K NO.	HEAT NO.	LOCATION	CHARPY TEST RESULTS								COMMENTS
			70 °F				40 °F				
			1	2	3	AVG	1	2	3	AVG	
M1-13	C47460	41 st St. // 72' S'S'CL of 28 th Ave. IFO C-Town Supermarket	15	16	17	16	12	7	7	9	Tested 3/20/96, S. Anders
M1-31	C50551	41 st St. // 152' S'S'CL of 28 th Ave. Opposite 28-13 41 st Street	10	15	11	12	8	7	7	7	Tested 3/20/96, S. Anders
M1-58	C44520	31 st Ave. // 82' W'W'CL of 35 th St. IFO 34-14 31 st Ave	27	23	28	26	15	15	16	15	Tested 3/15/96, S. Anders
M1-79	C45558	31 st Ave. // 132' E'E'CL of 35 th St. IFO 35-16 31 st Ave	4	4½	4	4	3	2½	2½	2½	Tested 3/15/96, S. Anders
M1-81	C45849	31 st Ave. // 113' E'E'CL of 32 nd St. IFO 32-12 31 st Ave	3	3	3	3	2½	2	3	2½	Tested 3/15/96, S. Anders
M1-90	C45546	41 st St. // 46' N'N'CL of 28 th Ave. IFO 25-95 28 th Ave	20	22	25	22	13	16	16	15	Tested 3/20/96, S. Anders
M2-5	C51458	34 th Ave. // 125' E'W'CL of 24 th St. IFO 24-14 34 th Ave	3½	4	3½	3½	2½	3	2½	2½	Tested 3/25/96, H. Goldenberg
M2-29	14515	31 st Ave. // 122' W'W'CL of 35 th St. IFO 34-10 31 st Ave	25	19	29	24	18	14	20	17	Tested 3/15/96, S. Anders
M2-32	5501860	41 st St. // 84' N'N'CL of 28 th Ave. Opposite 25-95 28 th Ave.	17	14	13	15	7	8	7	7	Tested 3/20/96, S. Anders
M2-38	567937	41 st St. // 328' N'N'CL of 28 th Ave. IFO 25-70 41 st St	23	25	23	24	18	15	18	17	Tested 3/20/96, S. Anders
M2-66	5463718	31 st Ave. // 56' E'E'CL of 31 st St. IFO 31-04 31 st Ave	49	36	40	42	17	29	22	23	Tested 3/15/96, S. Anders
M2-85	C23724	Crescent St. // 69' S'S'CL of 31 st Ave. IFO 31-04 Crescent St.	8	5½	6	6½	4	3½	3½	3½	Tested 3/25/96, H. Goldenberg
M2-93	C23720	41 st St. // 112' S'S'CL of 28 th Ave. IFO 28-12 41 st St.	24	28	27	26	18	20	18	19	Tested 3/20/96, S. Anders
Bell M1-78	C45558	Int. of 31 st Ave. & 33 rd St. Failed Pipe of 1/2/96	3	4	4	4	2½	2½	2½	2½	Tested 3/15/96, S. Anders
Spigot M2-16	C51458	Int. of 31 st Ave. & 33 rd St. Welded to Failed Pipe of 1/2/96	3	3½	2½	3	3	2½	2½	2½	Tested 3/15/96, S. Anders



Design Challenges

- Requirements
 - Design must be a **Full Structural Solution** while
 - Optimizing flow and minimizing impacts
- Impacts
 - Environmental Considerations
 - Heavily and densely populated community
 - Pollution and particulate matter
 - Financial Considerations
 - Local businesses
 - Heavy traffic for both residential and commercial vehicles
 - Community Considerations
 - Noise and traffic considerations for residences and businesses
 - Mix use commercial and residential zones



What Are the Options?

- Open-Cut
- Carbon Fiber Wrap
- Slip Lining
 - HDPE
 - Steel carrier pipe



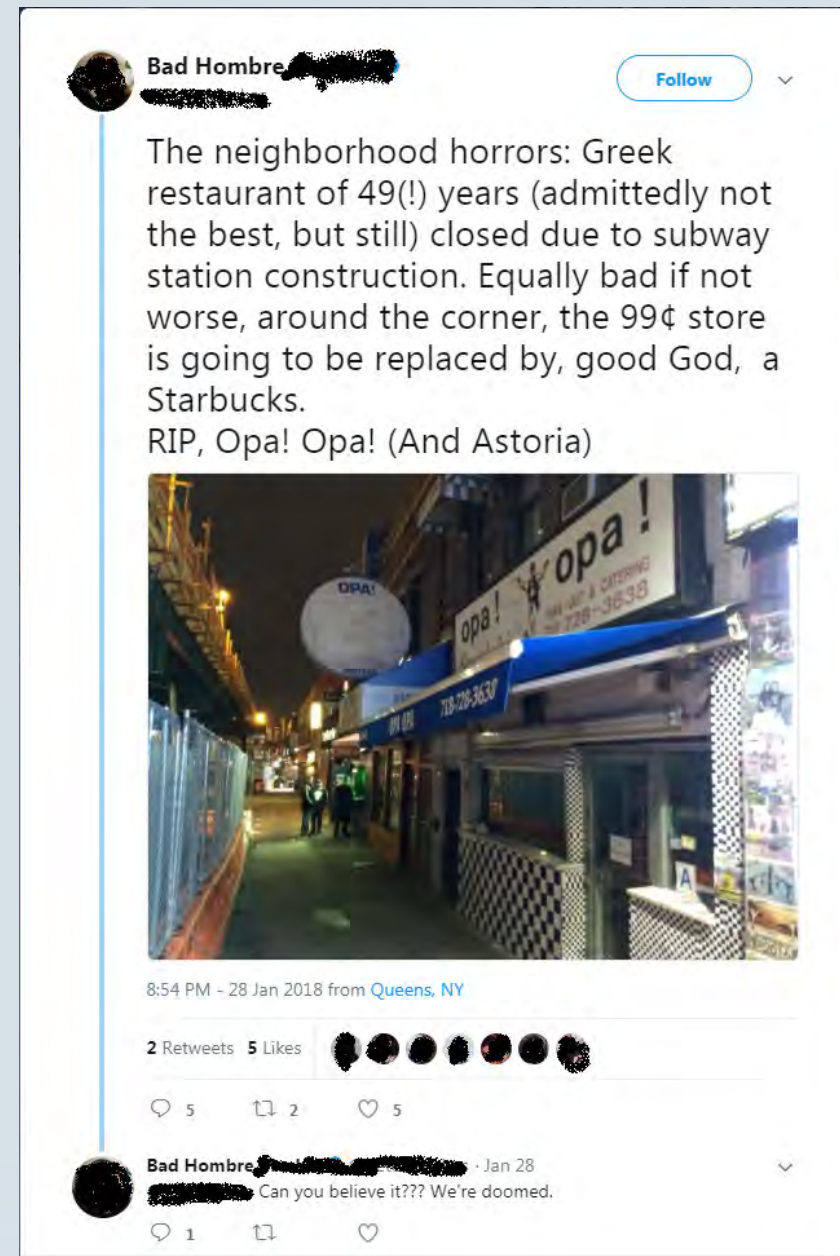
Open-Cut

Pros

- Full Structural Solution
- No Flow Capacity Loss

Cons

- Severe Socio-Economic Consequences
- Environmental Impacts
- Limited Work Hours
- Prolonged Schedule
- Expensive



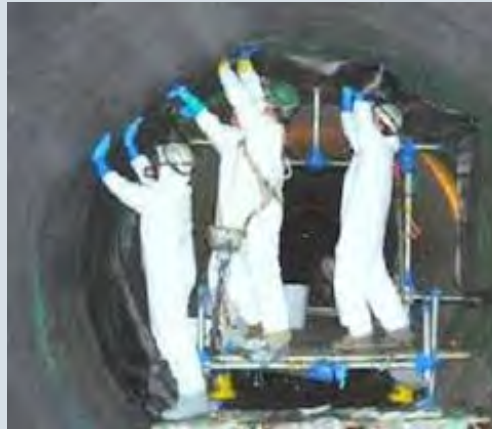
Carbon Fiber Wrap

Pros

- Minimal Disruption to the Community

Cons

- Only semi-structural solution
- Highly Labor intensive
- **Expensive**



Slip Lining with HDPE

Pros

- Successfully installed previously (Madison Avenue in Manhattan)
 - Proves slip lining as a feasible method for constructability in NYC.
- Drastically reduced construction duration and disturbance to community.

Cons

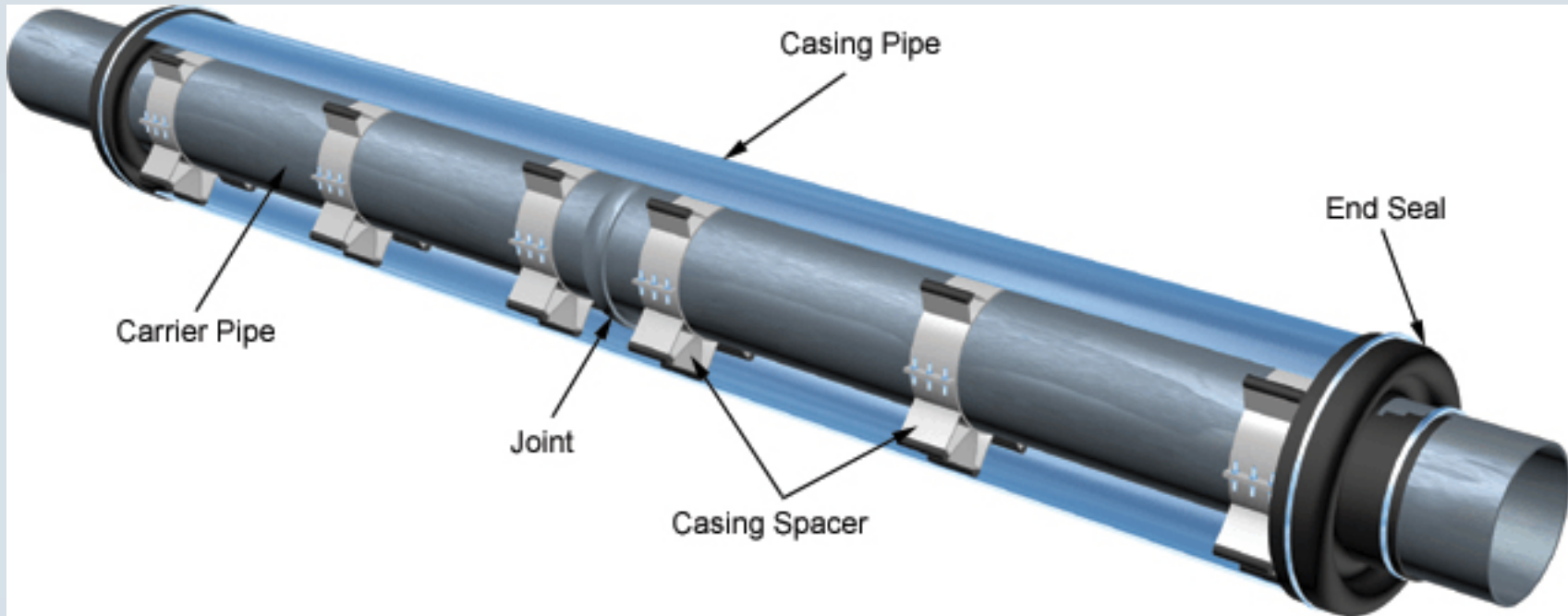
- Only semi-structural solution
- **HIGH** maintenance due to coupling failures



Lessons Learned

Design Solution

- DDC Design utilized steel pipe as a carrier instead of HDPE.
 - Steel pipe provides a fully structural solution with a full design life.
 - Steel pipe is **cheaper** than customized DIP.



Slip Lining with Steel Pipe



Pros

- Full Structural Solution
- Open-cut reduced by over **80%**
- Minimal loss of capacity
- Most cost effective method
- Reduce construction duration by upwards of **50%**

Cons

- Some loss of capacity
- Still some open-cut



Key Technical Considerations

- Pipe Parameters
 - 52-inch diameter steel pipe with ½ inch thickness
- Pipe Stops
- Casing Spacers
- Grouting of Annular Space
- Jacking and Receiving Pit Utilizations
- Constructability



Pipe Stops

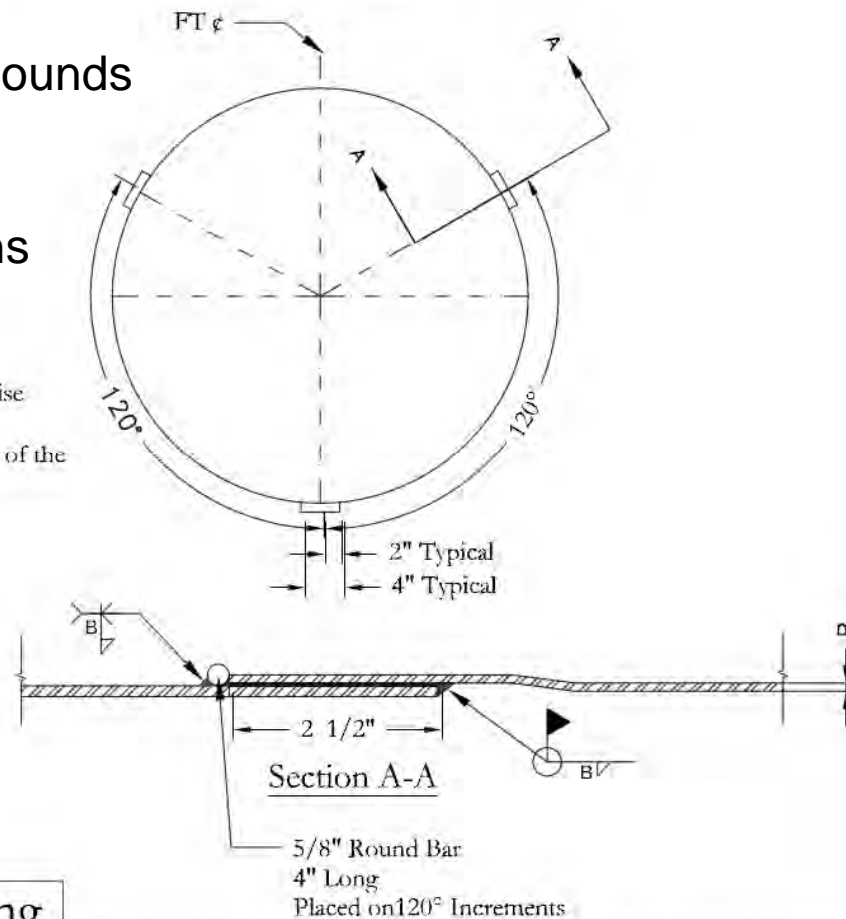
PIPE STOP FOR SLIPLINE PIPE

Max. load/pipe stop =
44,500 pounds

3 pipe stops per joint:
 $3 \times 44,500 = 66.75$ tons

Notes:

- All dimensions are in inches unless otherwise specified.
- All fillet welds to be the size of the thinner of the two materials being welded.



Pipe Lining and Coating

Pipe Stop Detail
Sample Drawing



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Casing Spacers

- **UHMWE PE Runners** utilized
 - Lower coeff. of friction
- **Constructability**
- **Corrosion Mitigation**

RUNNER

2" WIDE X 112" X 11" MOLDED POLYMER

4 TOP, 4 BOTTOM

Attached using (3) 3/8" welded steel studs/ locknuts recessed 1/2" below wearing surface of runner

Recess shall be filled with corrosion inhibiting filler.

RISERS

10 GA. (.134) HOT ROLLED PICKLED STEEL

MIG WELDED TO BAND

RISER 'A' = 1.00" TALL

RISER 'B' = J.3125" TALL

LINER

PVC LINER

HARDNESS 'A' 85-90

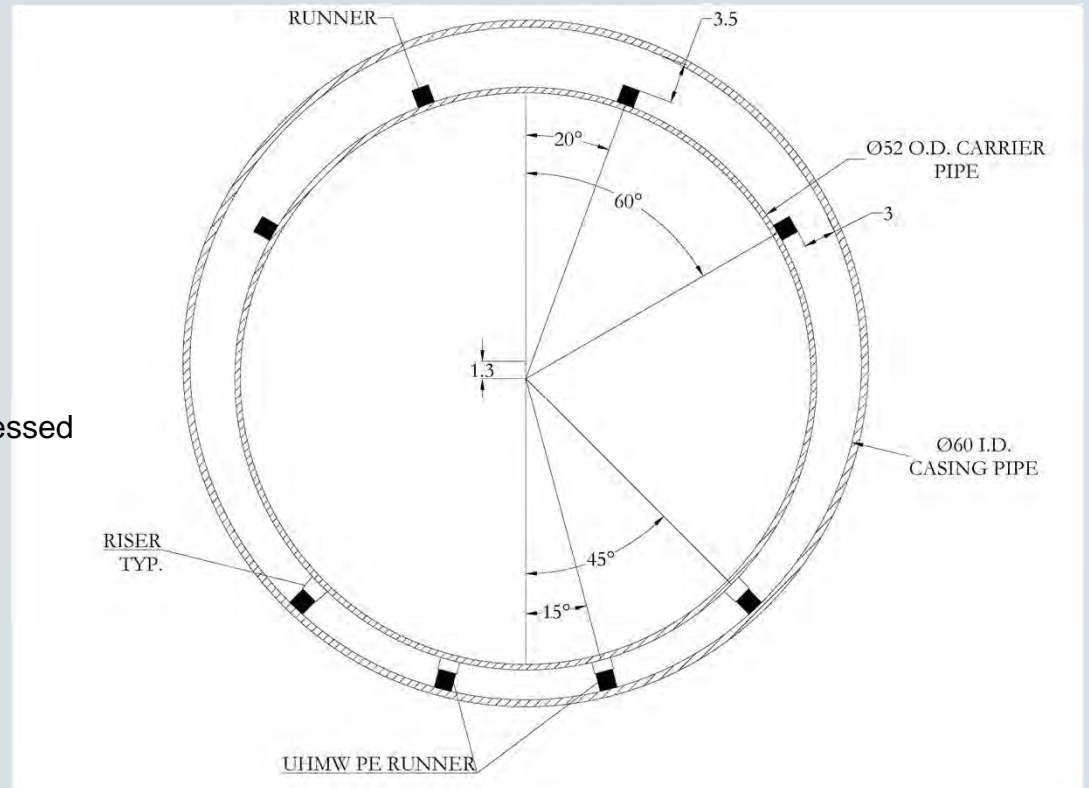
OPERATING TEMP, 140 F

DIELECTRIC STRENGTH - 60.000 VPM

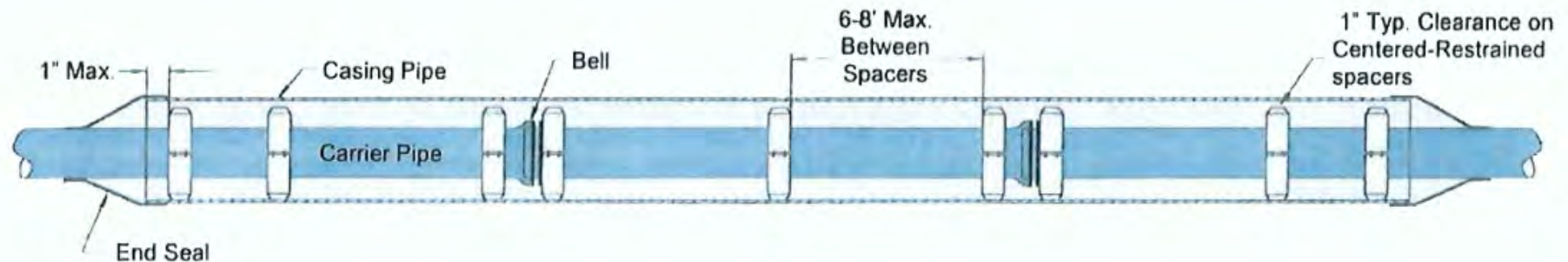
BAND

12" WIDE

12 GA. (.105") HOT ROLLED PICKLED STEEL 10-16 MIL THICK OF HEAT FUSED FLUIDIZED BED THER. "10 SET CROSS LINKED" EPOXY COATING" RIBBED FLANGES



Recommended Placement (For typical 20' joint)



A. General Carrier: One spacer shall be placed not more than one foot from each end of the casing and pipe joint. Subsequent spacers shall be a maximum of 7' intervals within the casing.

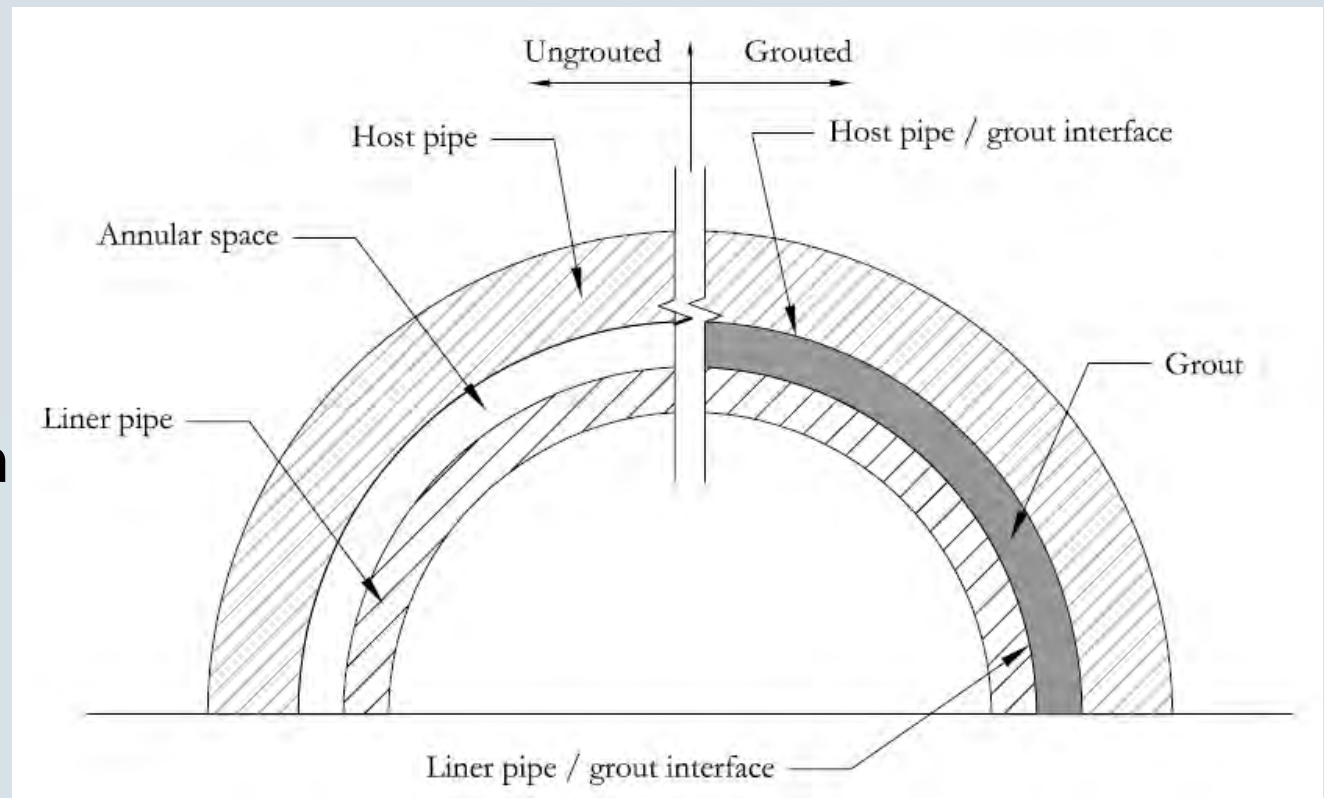
B. PVC Carrier: One spacer shall be placed on the spigot end of each segment at the line marking the limit of insertion into the bell. When the joint is complete, the spacer shall be in contact with the bells of the joint so that the spacer pushes the joint and relieves compression within the joint.



Grouting of Annular Space

Key Attributes Necessary to Grout Annular Space

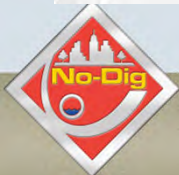
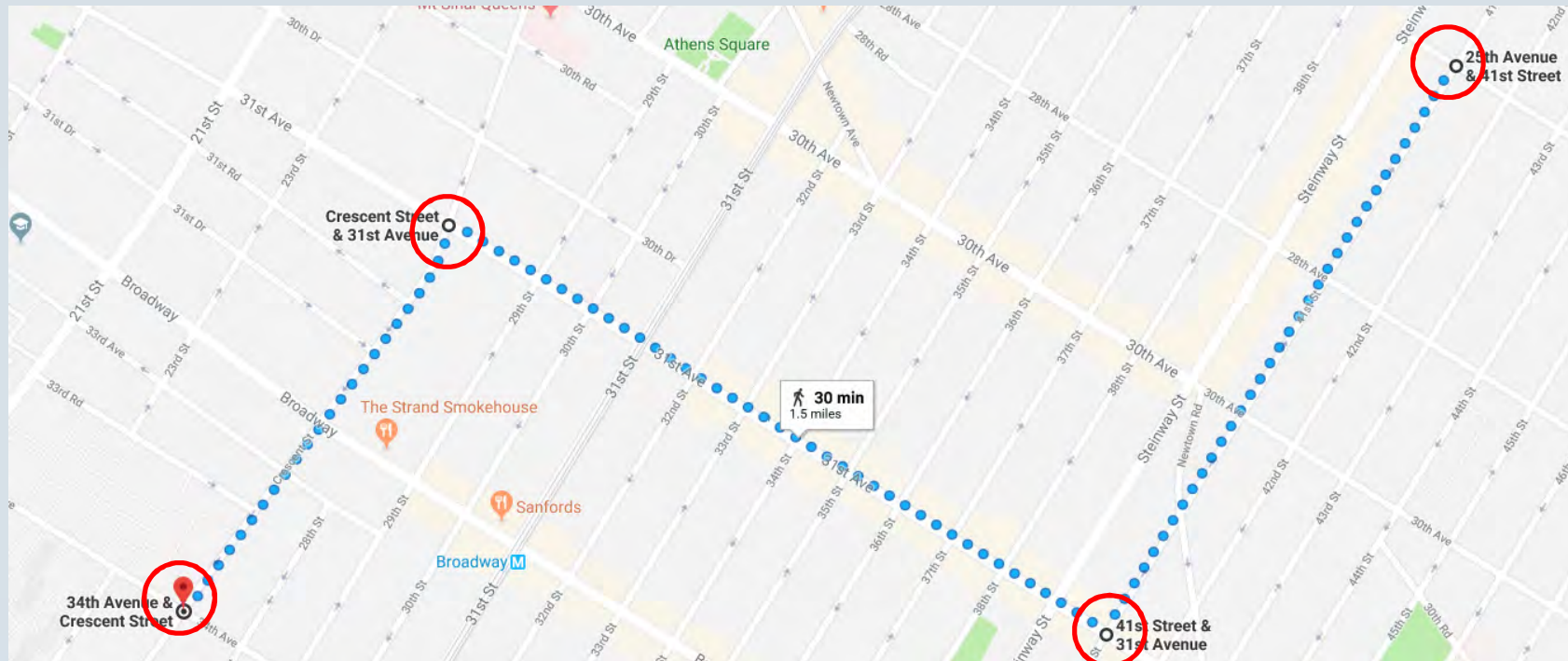
- High Flow Rate
- Lightweight
- 350-psi strength



Jacking & Receiving Pits

Open-cut Trench necessary only for:

- Negotiating bends
- Connections to Butterfly Valves
- Result = Over 80% Reduction of Open-Cut!

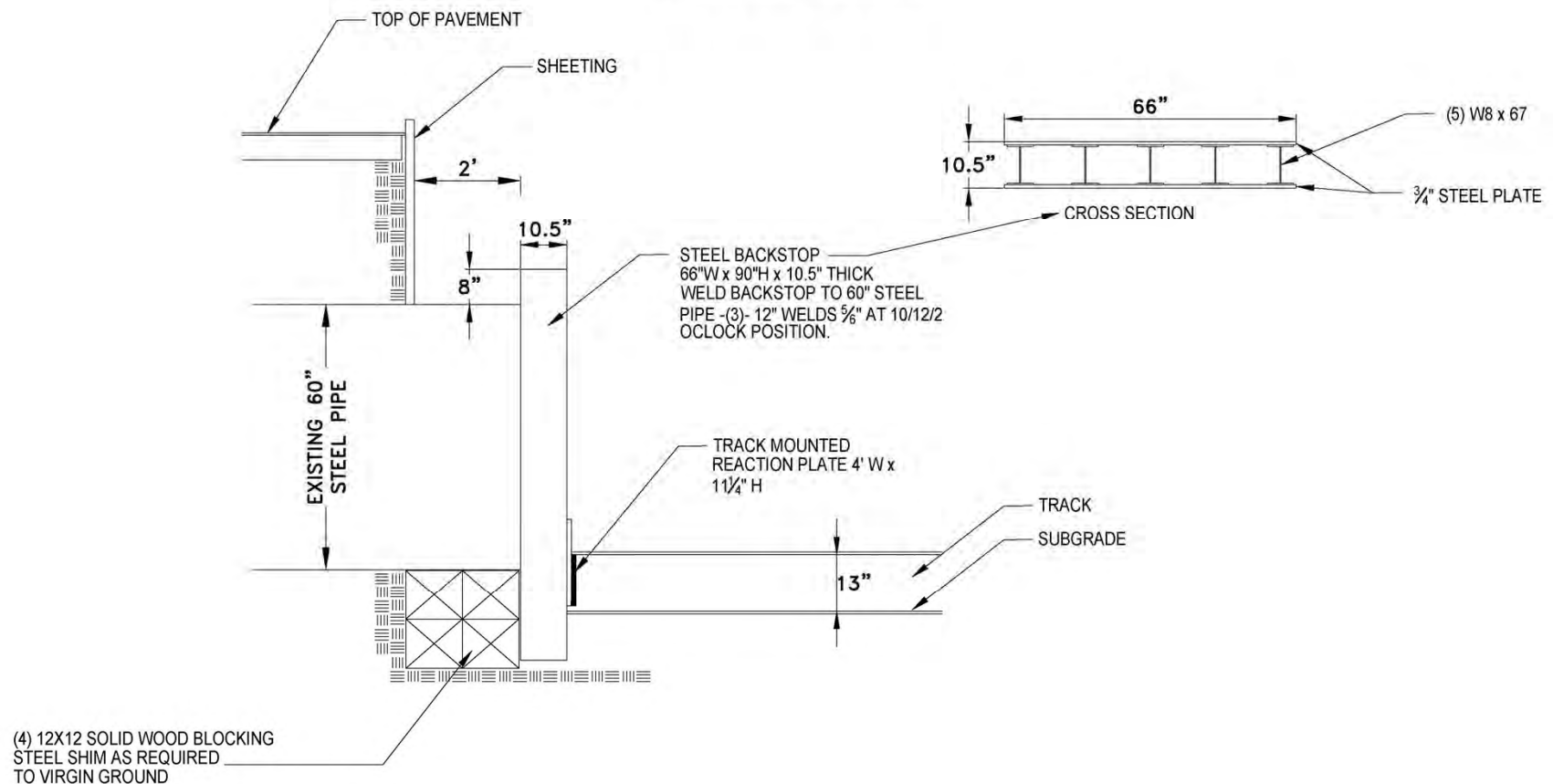


NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Jacking & Receiving Pits

TYPICAL INSERTION PIT DETAIL



Constructability – Push Force Requirements I

To establish the insertion push force requirements, the following factors were taken into consideration:

- Maximum Allowable Push Force
 - **66.75 tons** may be exerted on the 52" liner pipe
- Longest Slip Lining Run Length
 - **773'**
- Weight of 52" Liner Pipe & Spacers
 - **376.81 PLF.**
- Coefficient of Friction between Casing Spacers and Existing 60" host pipe.
Extensive testing resulted in the following:
 - 60" Host Pipe/ APS Runners, no lubrication - .54
 - 60" Host Pipe/ APS Runners with water lubrication - .52
 - 60" Host Pipe/ APS Runners with lubricant gel - .45
 - **60" Host Pipe/ APS Runners with lubricant soap - .32**
 - 60" Host Pipe/ APS Roller Spacers, no lubrication - .35



Push Force Requirements II

Maximum expected push force for slip line insertion is as follows:

Coefficient of Friction - .32

Length of longest Slip Lining Run – 773'

Weight of Pipe with Spacers - 376.8 PLF

$F_{max} = (\text{Coefficient of Friction}) \times (\text{Weight})$

$F_{max} = (.32) \times (773' \times 376.8 \text{ PLF})$

$F_{max} = 93,205 \text{ LB} = 46.60 \text{ Tons}$



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Jacking Unit JU-60 SL

- Designed to push a 52" steel pipe into an existing 60" steel pipe.
- The front plate of the sled is removable.
- Can be used for other sizes and pipe materials by simply changing the adapter plate.
- This machine has a sled that moves down the track, which is equipped with a winch that is connected to an anchor in the backstop.



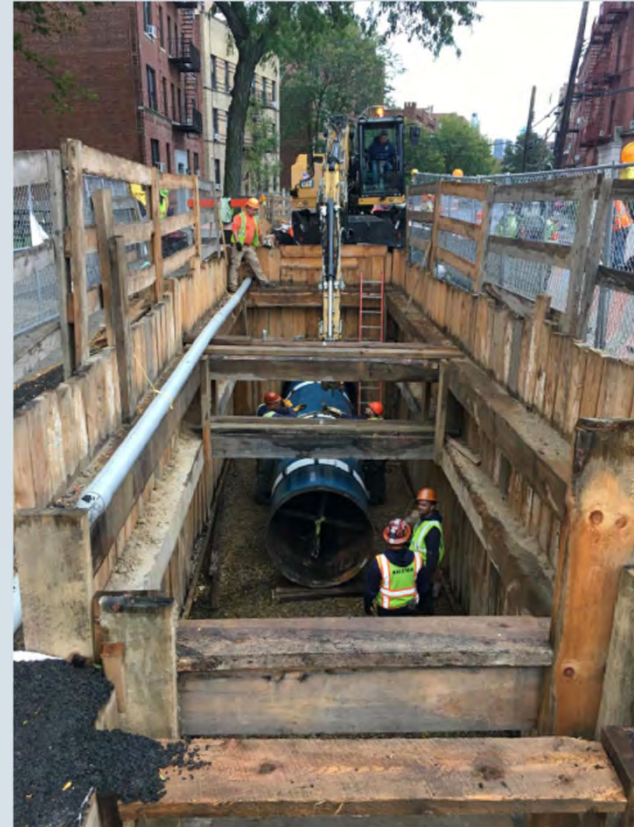
Test Pull Demonstration



Location: South side of 31st Avenue between 38th Street and Steinway Street

Operation: Test Run using 20.0 L.F. test pipe with runners.

In this test run, the pipe is pulled using a winch instead of pushed with the maximum allowable pushing force of 66.75 tons. The purpose of this test run was to test the friction of the runners and their performance against sliding.



Location: South side of 31st Avenue between 35th Street and 36th Street

Operation: Test Run using 20.0 L.F. test pipe with runners.



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Construction Video



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Schedule

Crescent Street

Starting date: June 26, 2017

Completion date: February 01, 2019

Duration

585 CCDs

31st Avenue

Starting date: August 21, 2017

Completion date: February 12, 2019

Duration

541 CCDs

Overlapping 529 CCDs

41st Street

Starting date: October 27, 2017

Completion date: June 24, 2019 (Original contract)

Final Completion date: December 23, 2019

Duration

606 CCDs

787 CCDs

Overlapping 473 CCDs

Crescent Street	Start June 26, 2017		February 01, 2019
31st Avenue	Start August 21, 2017		February 12, 2019
41st Street	Start October 27, 2017		December 23, 2019



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



Conclusion

Slip Lining of 52" Pipe into the 60" Trunk Main projected to:

- Provide fully structural solution with full design life
- Reduce open-cut trenching by at least **80%**
- Minimize environmental and socio-economic impacts
- Reduce construction duration by at least **50%**
- One-third the cost compared to Carbon Fiber Wrap
- One-half the cost compared to Open-Cut.

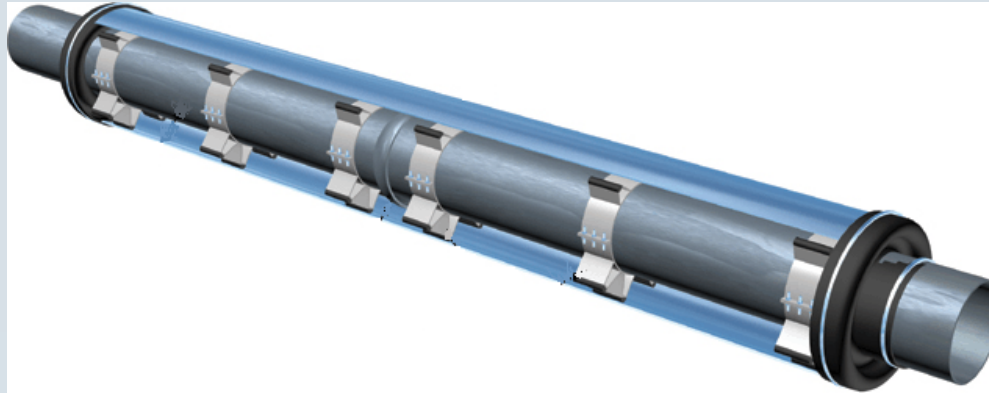


NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY



STRATEGIC SLIP LINE REHABILITATION OF NEW YORK CITY'S TRUNK WATER MAIN SYSTEM

ANY QUESTIONS?



MARIO VALENTI, P.E.

VALENTIM@DDC.NYC.GOV

THOMAS M. LEUNG, P.E., ESQ.

LEUNGT@DDC.NYC.GOV



Department of
Design and
Construction



NORTH AMERICAN SOCIETY FOR TRENCHLESS TECHNOLOGY

